

# ROLL PASS DESIGN EVAULUATION USING SOFTWARE APPLICATION

ARINDAM MUKHERJEE PROJECT MANAGEMENT CELL UNDP/GEF PROJECT (STEEL)

### **OBJECTIVE OF ROLL PASS DESIGN**

- Steel sections are generally rolled in several passes, whose number is determined by the ratio of initial input material and final cross section of finished product.
- The cross section area is reduced in each pass and form and size of the stock gradually approach to the desired profile.

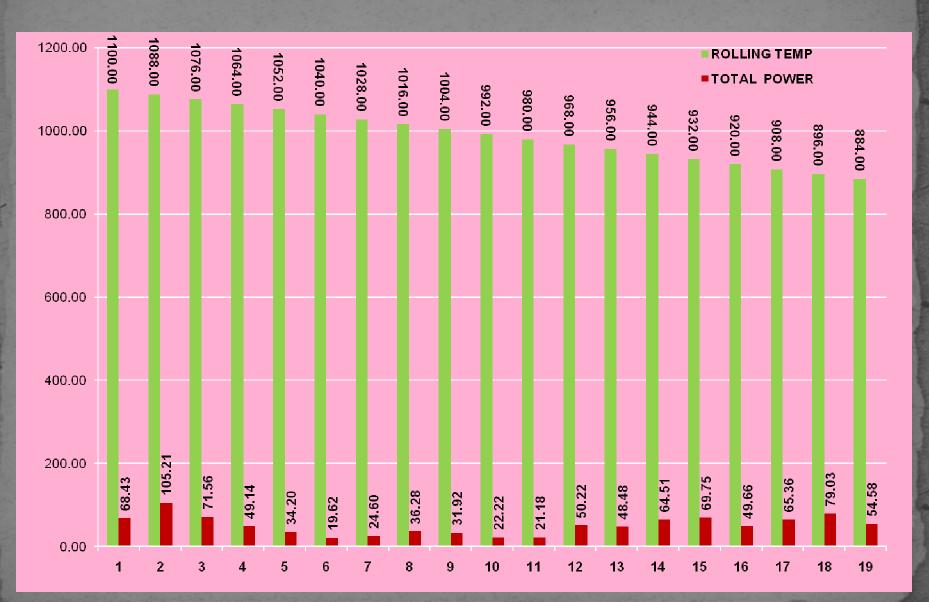
### **ROLLING PROCESS**

- Steel rolling consists of passing the material, usually termed the stock, between two rolls driven at the same peripheral speed in opposite directions (i.e. one clockwise and one anti-clockwise) and so spaced that the distance between them is somewhat less than the thickness of the section entering them.
- In these circumstances the roll grip the material and deliver it reduce in thickness, increased in length and probably somewhat increased in width.

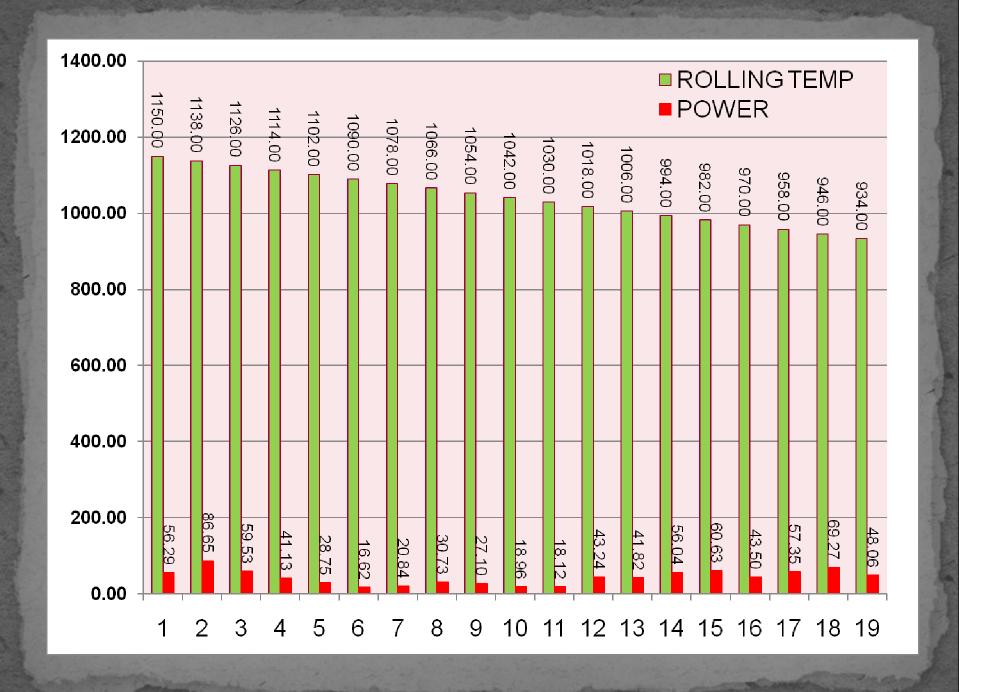
# OBJECTIVE OF ROLL PASS DESIGN

- Production of correct profile within tolerance limits with good surface finish (free from surface defects).
- Maximum productivity at lowest cost.
- Minimum roll wear.
- Easy working.
- Optimum energy utilization.

#### ROLL PASS IS BASED ON **CHARACTERISTICS CHARACTERISTICS** SPECIFICATION **OF FINISHED** OF INITIAL INPUT OF ROLLING MILL PRODUCT Wire Bars Rail BILLET BLOOM **Profiles** and structurals Dimension and weight of ٠ Dimension of section Number of stands billet Tolerances and Roll diameter Grade of steel specifications concerning Rolling speed Metal temperature before to mechanical properties Available power of and in the course of rolling Surface finish of rolled the drive motor product Available mill equipment Strength of rolls



IMPORTANCE OF TEMPERATURE



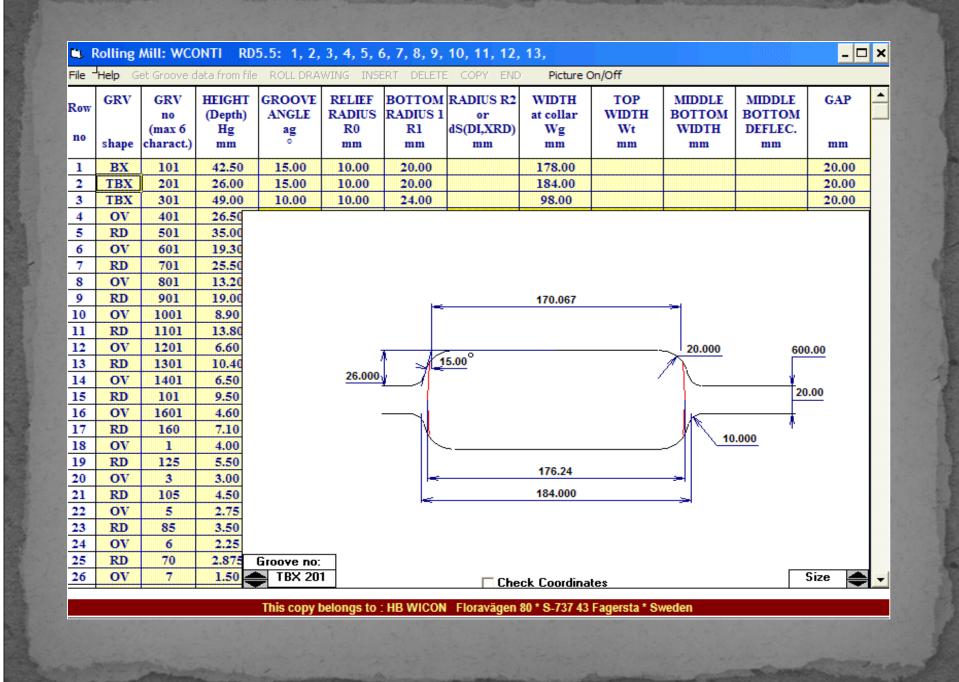
- Shape of sections in a particular passes must ensure a free metal flow in the roll gap/groove.
- Appropriate taper/groove angle in pass must be selected in order to avoid metal jamming in rolls.

TYPE OF PASS	% TAPER
Roughing pass	6 to 15
Forming pass	3 to 10
Finish pass	0.5 to 3.0%

#### Thumb rules for

#### **GROOVE ANGLE, RELIEF RADIUS, BOTTOM RADIUS & FITTING**

- Groove angle for box pass should be 8 to 10<sup>0</sup>.
- Relief radius for box pass should be 10 mm.
- Groove angle for diamond pass should be  $> 90^{\circ}$  .
- Relief radius for diamond should be around 18 mm.
- Groove angle for square pass should be 45<sup>0</sup>.
- Bottom angle for square pass should be around 90<sup>0</sup>.
- Relief radius for square pass should be 5mm .
- Groove angle for oval should be 60<sup>0</sup>.
- Relief radius for oval should be 5mm.
- Groove angle for intermediate round pass should be 60<sup>0</sup>.
- Groove angle for intermediate finish round pass should be 30<sup>0</sup>.
- Bottom radius for rounds is 1/2 of dia.
- Relief radius for rounds is 1/5<sup>th</sup> of bottom radius
- Relief radius for rounds in finish pass should be 1.5.
- Fitting from oval to round should be 0.3 to 0.7.
- For ovals width to height ratio should be < 3.0.



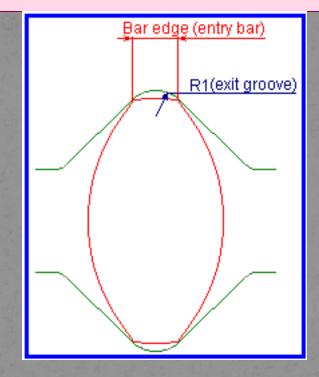
- The number and arrangement of passes in particular roll stand should assure the most uniform possible exploitation of all the passes in each stand.
- Uniform draught in last passes & different draught in early forming passes of profile , where the section is large & metal is hot.
- Draught should be distributed so as to ensure as far as possible uniform wear and to avoid overloading of drive installations and rolls.

• Rolls should easily grip the material being rolled .

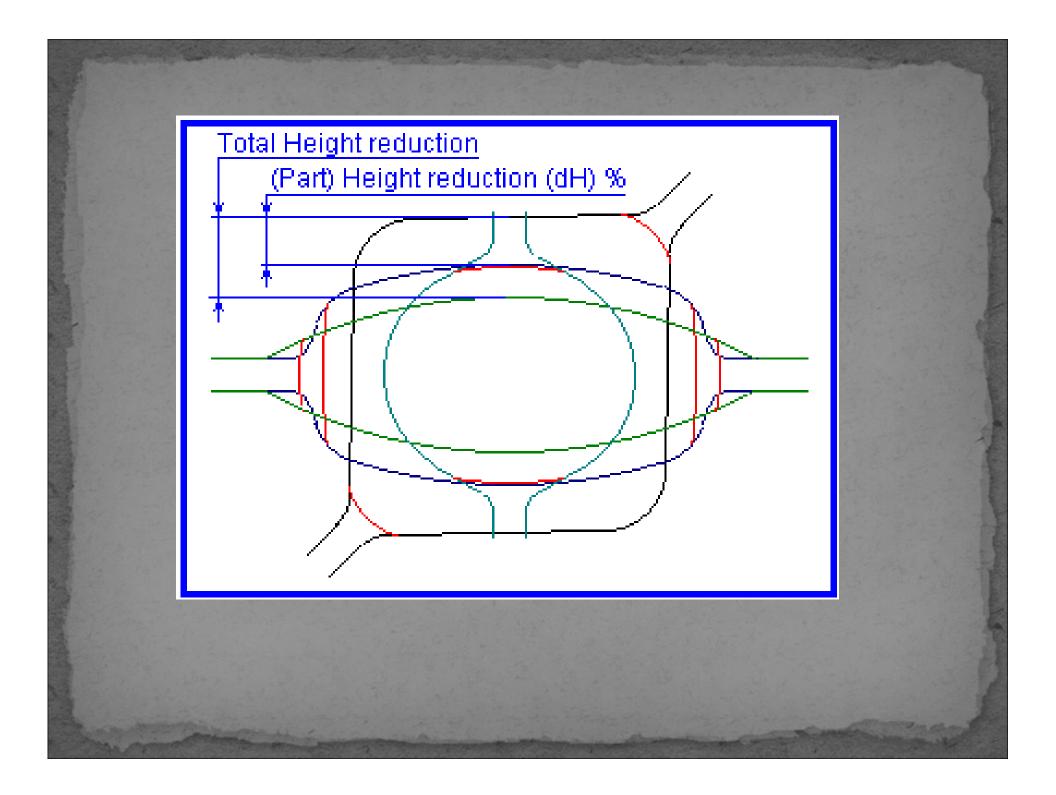
Rolls Finish		Max. Angle of Bite (in degrees) with reference to speed of mill												
	0	0.5	1	1.5	2	2.5	3	3.5						
Smooth	25.5	24.5	23.5	22.5	19.5	16	12	9						
Edged passes	29	27.5	26	24.5	21	17	12	7						
Ragged	33	32	31	30	28	26	24	21						

• Pass filling should be correct.

#### Fitting = Bar edge<sub>(entry bar</sub>)/2 \* Groove bottom radius<sub>(exit groove)</sub>



The **Fitting** parameter should be 0.3 < Fitting < 0.7 to avoid problems with bad surface quality and bad wearing conditions of the groove bottom.



 An optimum number of passes should be used.

If, Too greater in number  $\rightarrow$  Lower the out put of the roll stand Too smaller in number  $\rightarrow$  Cause excessive roll wear

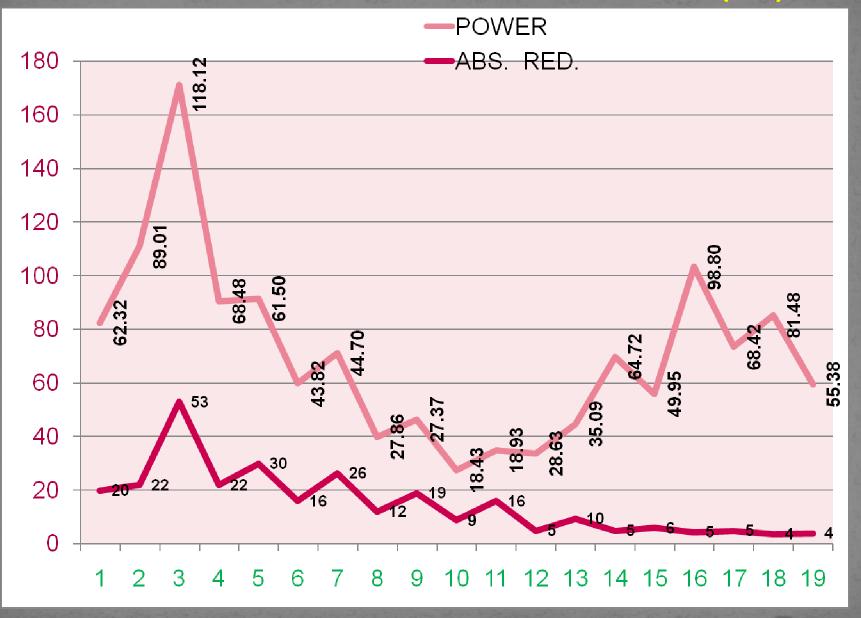
Danger of roll fracture or rolling defect

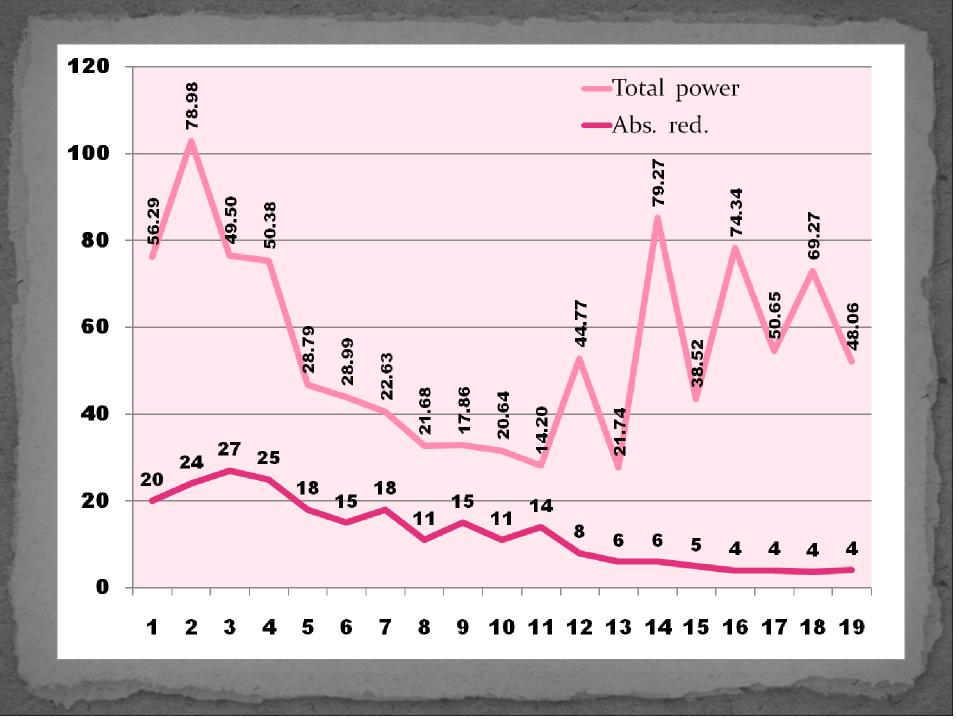
	ingation	LUEITICIEI	•					o. of Passes	PASSES
			•	-		duction			
Pass No.	5	10	15	20	25	30	35	40	Input Size = 200x200 mm
1	1.053	1.111	1.177	1.250			1.538	1.667	
2	1.108	1.235	1.384		1.777		2.365	2.779	Finish Product = 50x50 mm
3	1.167	1.372	1.628		2.369		3.638	4.63	
4	1.228	1.524	1.915			4.170	5.595	7.72	$\lambda_{t = 200 \times 200/50 \times 50} = 16$
5	1.293	1.694	2.253			5.96	8.606	12.87	$r = 200 \times 200 / 50 \times 50 = 16$
6	1.361	1.883	2.650	3.815	5.610	8.52	13.24	21.5	With 05.9/ Dada In every name offer
7	1.432	2.092	3.117	4.77	7.48	12.17	20.36	35.8	With 25 % Redn. In every pass after
8	1.508	2.324	3.667	5.96	9.97	17.39	31.31	59.6	th a th a
9	1.587	2.582	4.313	7.45	13.29	24.8	48.15	99.4	$_{9}^{\text{th}}$ pass $\lambda_{\text{t}}$ = 13.29 and after 10 h pass $\lambda_{\text{t}}$
10	1.670	2.868	5.073	9.31	17.71	35.5	74.06	165.7128	=17.71.
11	1.758	3.187	5.967	11.64	23.61	50.7	114	276.2432	10 passes will be sufficient with redn. Somewhtat
12	1.851	3.540	7.019	14.55	31.5	72.5	175	460.4974	less than 25 %.
13	1.948	3.933	8.256	18.19	42.0	104	269	767.6492	
14	2.050	4.370	9.711	22.74	55.9	148	414	1279.671	
15	2.159	4.855	11.423	28.42	74.6	212	637	2133.212	Last pass = 5% , $\lambda_{t=1.053}$
16	2.272	5.394	13.445	35.53	99.4	302	980	3556.064	
17	2.392	5.992	15.824	44.41	132	432	1508	5927.959	Preleader =10% , $\lambda_{t}$ = 1.111
18	2.518	6.658	18.625	55.51	177	617	2319	9881.908	′°t = 1.111
19	2.651	7.397	21.922	69.39	235	882	3566		(0)
20	2.790	8.218	25.802	86.74	314	1261	5484		=1.053x1.111=1.168
21	2.938	9.130	30.369	108.4	418	1802	8435		
22	3.092	10.143	35.744	135.5	558	2575			$\lambda_{t=16/1.168=13.7}$
23	3.255	11.269	42.071	169.4	743	3679			
24	3.427	12.520	49.497	211.8	991	5257			With 30% redn. 13.7 can be achieved after 7 pass
25	3.607	13.910	58.257	264.7	1321	7513			th or we can say 8 pass.

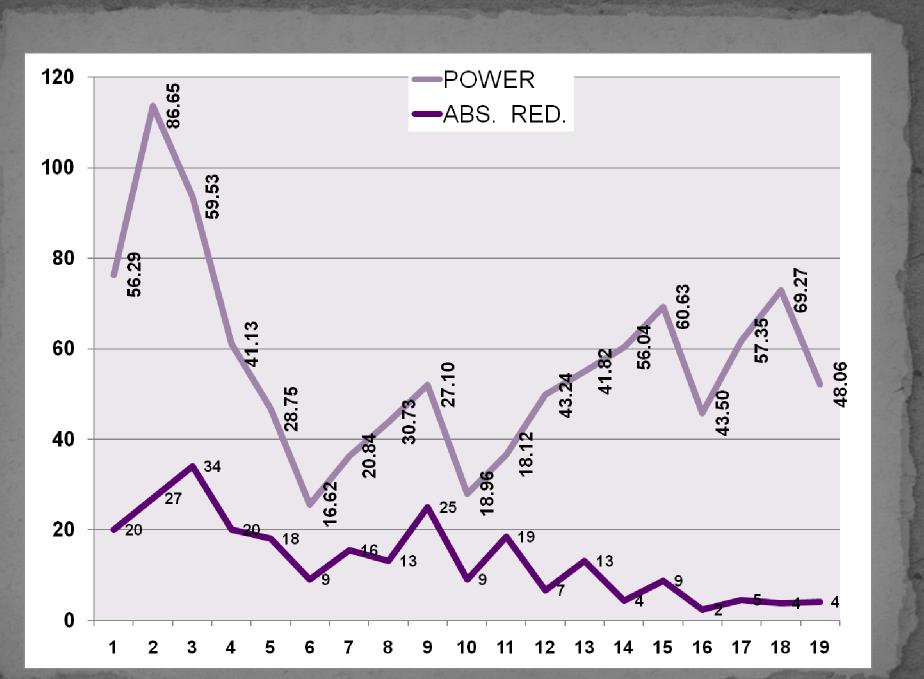
### **EVALUATION BASED ON ABSOLUTE REDUCTION**

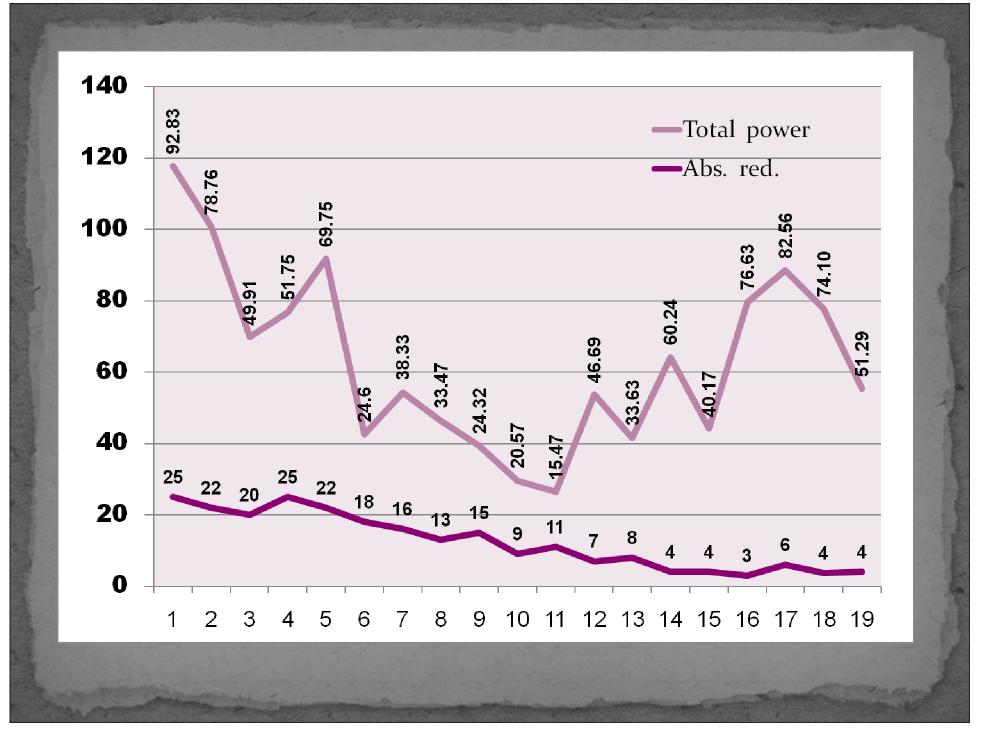
Pass	Pass	Initial	Initial	Initial	Final	Final	Final	Mean	Abs.	Pass wise
no	Shape	width	height	Area	width	height	Area	width	red.	Power(Kw)
										Required for
										Deformation
		В	Н	Fo	b	h	F1	Bm	dh	
		mm	mm	mm2	mm	mm	mm2	mm	mm	
1	Вох	100.00	100.00	9940.00	110.00	80.00	7920.00	105	20	62.32
2	Вох	110.00	80.00	7920.00	125.00	58.00	6525.00	118	22	89.01
3	Square	58.00	125.00	6525.00	72.00	72.00	5184.00	65	53	118.12
4	Вох	72.00	72.00	5184.00	86.00	50.00	3870.00	79	22	68.48
5	Square	50.00	86.00	3870.00	56.00	56.00	3136.00	53	30	61.50
6	Вох	56.00	56.00	3136.00	66.40	40.00	2376.00	61	16	43.82
7	Square	40.00	66.40	2376.00	40.00	40.00	1600.00	40	26	44.70
8	Oval	40.00	40.00	1600.00	48.00	28.00	1055.04	44	12	27.86
9	Square	28.00	48.00	1055.04	29.00	29.00	841.00	29	19	27.37
10	Oval	29.00	29.00	841.00	36.00	20.00	565.20	33	9	18.43
11	Square	20.00	36.00	565.20	20.00	20.00	400.00	20	16	18.93
12	Oval	20.00	20.00	400.00	24.00	15.00	282.60	22	5	28.63
13	Square	15.00	24.00	282.60	14.50	14.50	210.25	15	10	35.09
14	Oval	14.50	14.50	210.25	18.00	9.50	134.24	16	5	64.72
15	Round	9.50	18.00	134.24	12.00	12.00	113.04	11	6	49.95
16	Oval	12.00	12.00	113.04	15.00	7.50	88.31	14	5	98.80
17	Round	7.50	15.00	88.31	10.00	10.00	78.50	9	5	68.42
18	Oval	10.00	10.00	78.50	12.00	6.30	59.35	11	4	81.48
19	Round	6.30	12.00	59.35	8.00	8.00	50.24	7	4	55.38
Man Prop		at the state	ALL STATE	Constantine of the second	NAME OF CASE OF CASE	STREET, STREET				

#### **ABSOLUTE REDUCTION & POWER REQUIRED (KW)**

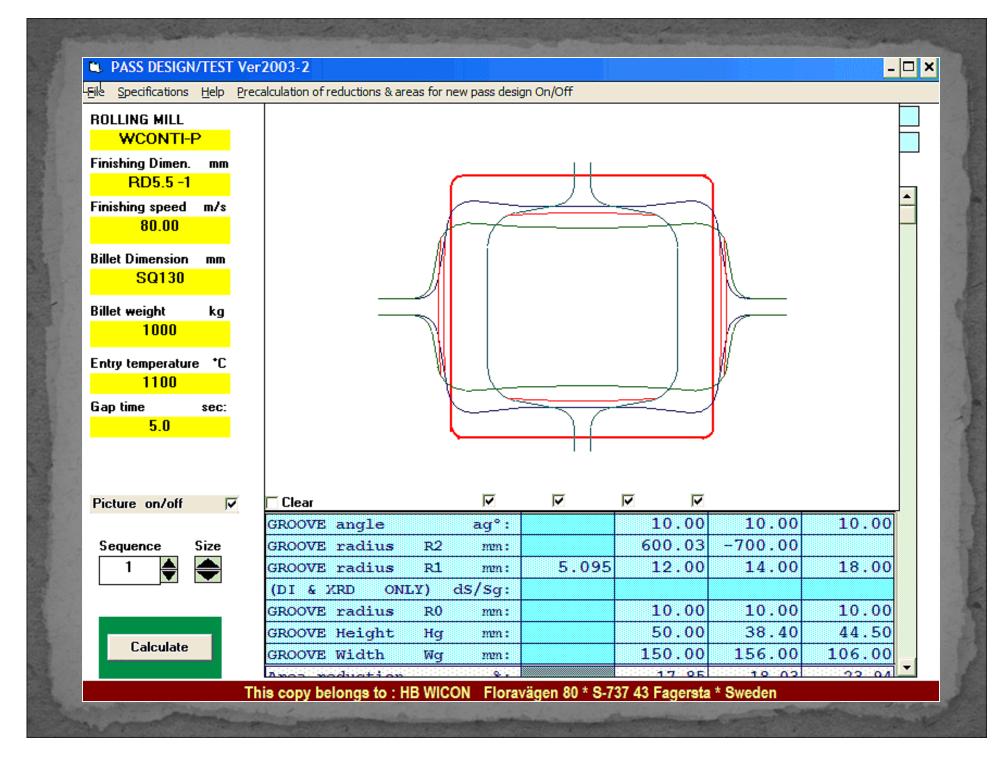


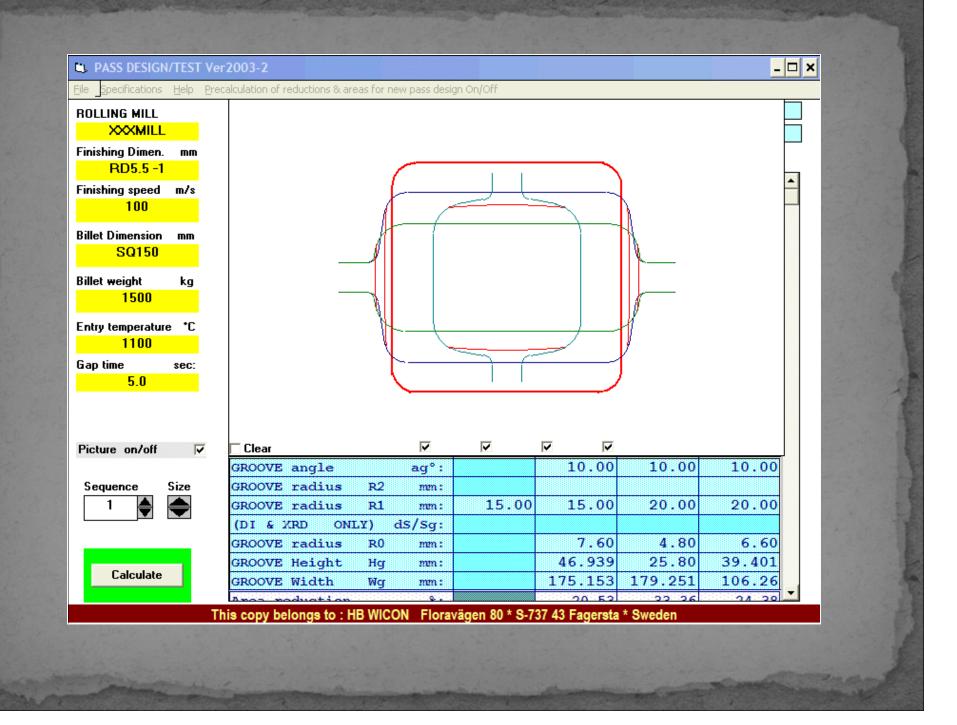


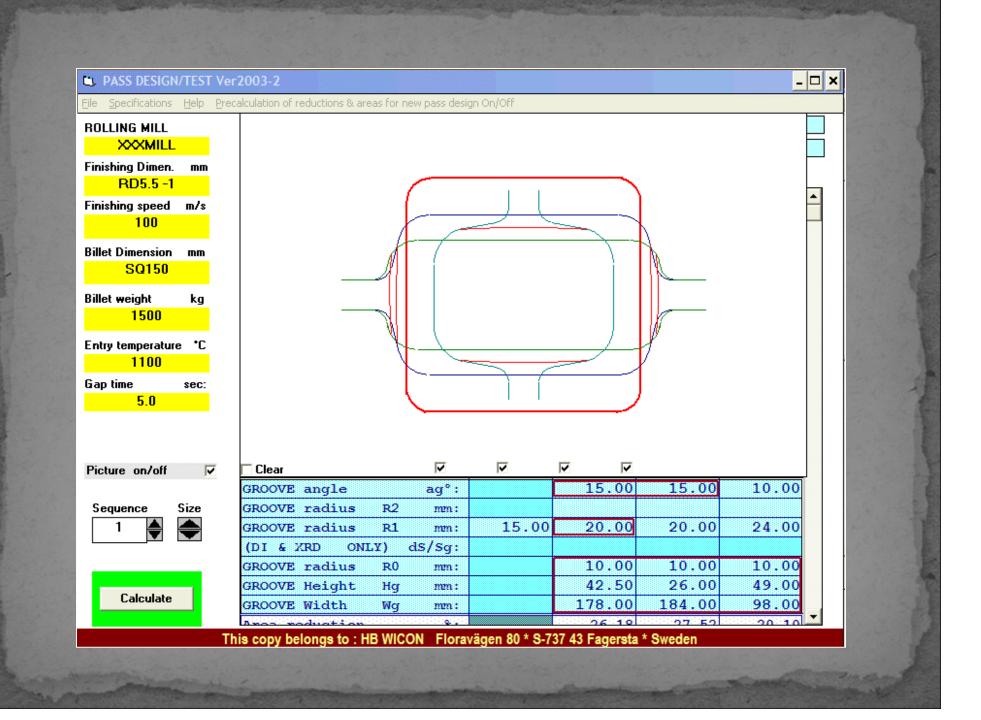


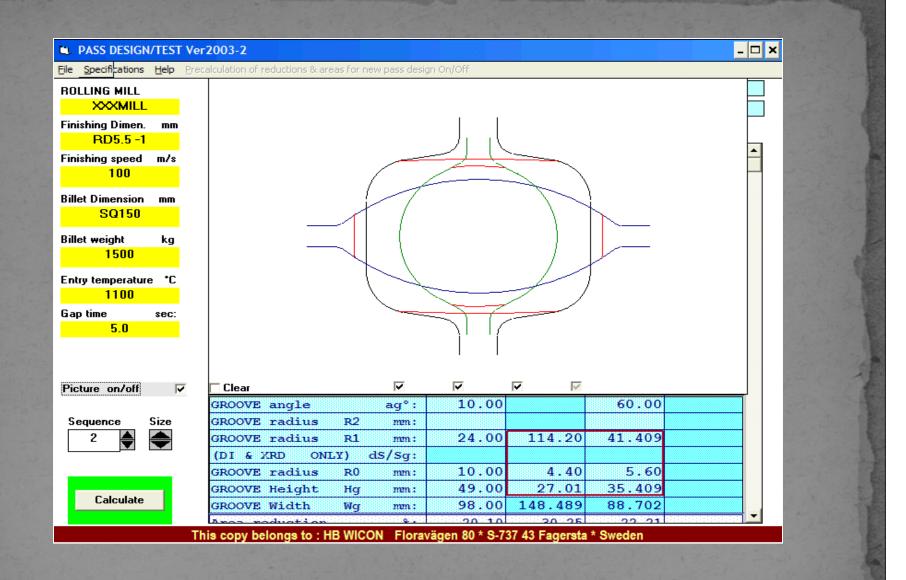


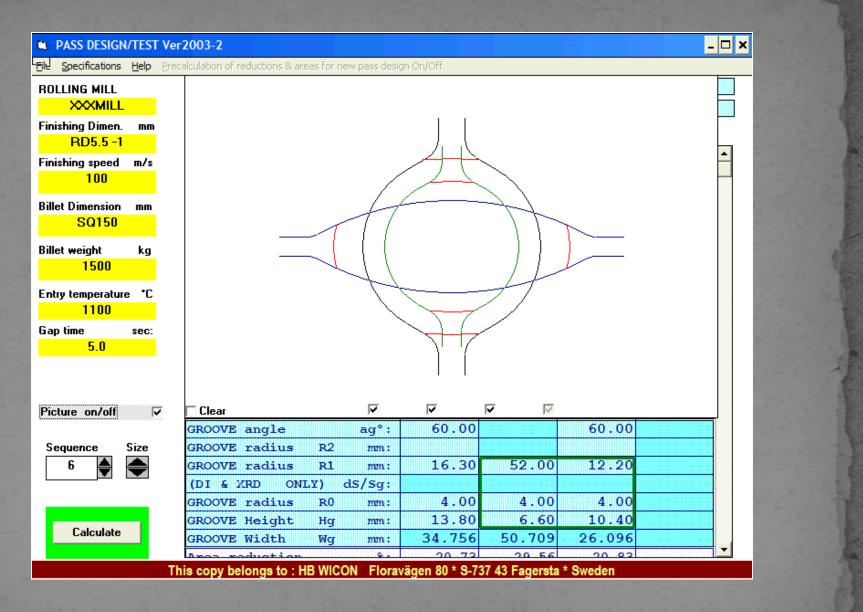












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🕒 WCONTI 🛛 Rolling sche	edule: RD	5.5-111	Material	: 3. Carb	on Steel	1.00	C (*1.00)			_ 🗆	×
File -Help Flow Stress Properties	Rearrange	ments on/of	f Change d	ata on/off	Graphs on/o	off Picture	on/off				
PASS / SEQUENCE no	18/9	19/9	20/10	21/10	22/11	23/11	24/12	25/12	26/13	27/13	
STAND no	15-1	15-2	15-3	15-4	15-5	15-6	15-7	15-8	15-9	15-10	
GROOVE no	OV	RD	OV	RD	OV	RD	OV	RD	OV	FRD	
Billet:S0152.8	<b>I</b>	125	3	105	5	85	6	70	7	55	
ROLL GAP (empty) mm	1.67	2.13	2.08	1.44	0.99	1.44	0.70	1.09	1.21	1.45	
ROLL GAP(active) mm	2.20	2.40	2.40	1.60	1.20	1.50	0.80	1.05	1.20	1.30	
PRIOR Gap -"- mm											
Gap DIFF"- mm											
Bar HEIGHT Hb HOT	10.20	13.40	8.40	10.60	6.70	8.50	5.30	6.80	4.20	5.55	
Bar WIDTH Wb HOT	20.73	12.80	16.29	10.58	13.28	8.63	10.98	6.99	9.09	5.52	
Inscr. circle Si HOT											
Elongation	1.253	1.238	1.237	1.238	1.232	1.250	1.230	1.249	1.238	1.242	
ROLL DIAMETER mm	216.0	216.0	216.0	216.0	216.0	216.0	216.0	216.0	216.0	216.0	
EFFECTIVE dia. mm	223.67	222.39	224.29	223.11	223.87	224.81	224.44	225.15	226.18	225.67	
MOTOR revolution rpm	1356	1356	1356	1356	1356	1356	1356	1356	1356	1356	
SPEED m/sec	14.5	18.0	22.2	27.5	33.9	42.3	52.1	65.0	80.5	100.0	
Loop/Pull MIN m or %	- 0.2%	- 0.2%	- 0.2%	- 0.2%	- 0.2%	- 0.2%	- 0.2%	- 0.2%	- 0.2%	T. Prod.	
Loop/Pull CAL. m or %	- 0.9%	- 1.3%	- 1.1%	- 1.6%	- 1.3%	- 1.6%	- 1.5%	- 1.5%	- 2.4%	61.62	
Loop/Pull MAX m or %	- 2.0%	- 2.0%	- 2.0%	- 2.0%	- 2.0%	- 2.0%	- 2.0%	- 2.0%	- 2.0%	tons/h	
ENTRY temperature °C	1029	1030	1032	1036	1043	1053	1065	1080	1096	1116	
LOAD kN	112	72.0	83.3	59.5	71.2	49.7	59.3	40.1	48.9	30.4	
TORQUE kNm	2.19	1.57	1.40	1.16	1.12	0.90	0.86	0.67	0.65	0.46	
POWER kW	284	254	278	286	339	337	397	387	463	409	
Power MAX kW	=====>	>	=====>	=====>	=====>	>	=====>	====>	>	3833	
Power MEAN kW	>	>	>	>	>	>	>	>	>	3719	
Power AVAILABL kW	>	====>	=====>	=====>	>	=====>	====>	====>	>	4000	
Angle of Bite °	13.7	15.4	11.7	13.5	11.0	12.3	10.2	11.4	9.3	10.5	
Bar Area HOT mm <sup>2</sup>	168.2	135.9	109.9	88.72	72.03	57.63	46.86	37.53	30.30	24.40	
Bar length HOT m	1196	1481	1832	2268	2795	3494	4299	5369	6652	8264	
Spread Coefficient :	1.30	1.20	1.30	1.20	1.30	1.20	1.30	1.20	1.30	1.20	
! OBSERVATIONS !						+T			-L		-
•										•	Ρ
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# **ROLLING OBSERVATIONS**

- +T Risk of tilting in the next groove due to too large width
- -T Risk of tilting in the next groove due to too small width
  - +F The ratio Bar Edge/Groove Bottom Diameter of the next groove is >0.7
- +O Overfilling (Bar width>Groove Width)
- +W Width of finishing dimensions is more than 1.5% TOO LARGE
  - -W Width of finishing dimensions is more than 1.5% TOO SMALL
  - +D Sb,Db or Hb of finishing dimensions is more than 1.5% Too Large
- -D Sb,Db or Hb of finishing dimensions is more than 1.5% Too Small
- +L Loop Growth by repeater rolling is TOO LARGE . Tension by block rolling is TOO SMALL
- -L Loop Growth by repeater rolling is TOO SMALL. Tension by block rolling is TOO LARGE
- -N Motor revolution is below the base revolution . Full power is not available

E.		-	- the		-			20	3		12	1	1	- 2	240	1		225	- 25		6 2 4			25-3	100	120	1.1	
				<b>-</b>		- 1			Roll			Linea	Angl	Coeff					Relativ		Mean	<b>.</b>	<b>.</b>	_	-	Powe		
Pass	Initial	Initial	Initial	Final	Final	Final	Mean	Abs.	dia.	Work	Roll	r	e	of	Rolling	Metal	of	of	e	Sigma	sp.	Rolling	Rolling	Power	Torque	r for	Total	Cum
	width	height	Area	width	height	Area	width	red.	max.	dia	rpm		of bite	draug ht		comp.		viscosi ty	deform rate		rolling pr.	force		for defor m.	for friction	fricti on	power	Power
1	В	н	Fo	b	h	F1	Bm	dh	Dk	Dwk	n	v	<	/u	t		F	n/	U	0-	р	Р	Ma	Na	Mn	Nn	N	N
no	mm	mm	mm2	mm	mm	mm2	mm	mm	mm	mm	rpm	m/s			<u>а</u> С	Comp.		kgf s/m	n 1/s	kgf s/m 2	kgf/m m 2	Т	kgm	kW	kgm	kW	kW	kW
						mmz					ipin	11/3	ueg.		00	comp.		2	1/3	2	111 2	1	Kgili	KW	Kgili	K VV	KW	K VV
																												-
1	100.00	100.00	9940	105	75	7875	103	25	460	377	90	0.42	19	1.12	1125	2.30	0.49	0.03	1.60	7.70	8.98	69.82	5029.41	90.88	1059.82	1.95	92.83	
2	105.00	75.00	7875	109	53	5724	107	22	460	399	90	0.42	18	1.17	1113	2.30	0.49	0.03	2.05	6.60	8.14	61.93	4184.92	77.03	940.07	1.73	78.76	
3	53.00	109.00	5724	92	92	4265	72	17	460	380	90	0.42	16	1.16	1101	2.30	0.50	0.03	1.15	6.88	7.89	35.83	2133.64	48.91	543.95	1.00	49.91	
4	65.00	65.00	4265	95	50	2980	80	15	460	402	90	0.42	15	1 20	1089	2.30	0.51	0.03	1.88	7.15	8.99	42.24	2356.80	50.57	641.15	1.18	51.75	
10																												
5	50.00	95.00	2980	65	65	2025	58	30	460	396	90	0.42	21	1.21	1077	2.30	0.51	0.03	1.91	7.43	8.91	42.56	3355.59	68.56	646.03	1.19	69.75	
6	45.00	45.00	2025	66	36	1487	55	9	460	412	90	0.42	11	1.17	1065	2.30	0.52	0.03	2.07	7.71	10.26	25.79	1114.91	23.88	391.57	0.72	24.60	
7	36.00	66.00	1487	46	46	1056	41	20	460	412	90	0.42	17	1.19	1053	2.30	0.52	0.03	2.24	7.98	10.32	28.71	1851.96	37.53	435.88	0.80	38.33	
8	32.50	32.50	1056	48	19	731	40	13	460	424	90	0.42	14	1.20	1041	2.30	0.53	0.04	3.90	8.26	13.16	29.06	1515.63	32.66	441.21	0.81	33.47	
9	19.00	48.00	731	33	33	527	26	15	460	426	90	0.42	15	1.18	1029	2.30	0.54	0.04	2.73	8.53	11.98	18.41	1043.51	23.81	279.54	0.52	24.32	
10	23.00	23.00	527	36	14	396	30	9	460	436	90	0.42	11	1 1 5	1017	2.30	0.54	0.04	4.53	8.81	15.62	20.97	906.38	19 99	318.33	0.59	20.57	
6								-																				267.61
	14.00	36.00	396	25	25	306	19	11	460	435	90	0.42	13	1.14	1005	2.30	0.55	0.04	3.09	9.09	13.73	13.53	653.94	15.09	205.42	0.38	15.47	367.61
12	17.50	17.50	306	27	11	266	22	7	330	312	180	1.70	11	0.32	993	2.30	0.55	0.04	23.91	9.36	16.40	11.91	373.78	45.36	129.74	1.33	46.69	
13	10.89	26.50	266	19	19	179	15	8	330	312	180	1.70	12	1.22	981	2.30	0.56	0.04	16.05	9.64	14.44	7.62	256.44	32.78	82.96	0.85	33.63	80.32
14	13.36	13.36	179	19	9	135	16	4	260	247	290	4.40	11	1.15	969	2.30	0.57	0.04	72.09	9.913	17.17	6.62	149.61	58.31	56.76	1.92	60.24	
15	9.00	19.00	135	15	15	106	12	4	260	257	290	4.40	10	1.13	957	2.30	0.57	0.04	47.16	10.189	15.16	4.23	94.46	38.94	36.30	1.23	40.17	100.41
16	10.43	10.43	106	16	7	90	13	3	280	271	380	7.56	9	1.08	945	2.30	0.58	0.05	131.59	10.465	19.98	5.66	115.20	73.81	52.29	2.82	76.63	
17		16.00	90	10	10	78	9	6	280	278					933				120.34				129.96			2.35		159.19
1/	1.15	10.00	90	10	10	/0	9	0	200	270	500	1.50	10	1.08	933	2.50	0.58	0.05	120.34	10.741	10.99	4.72	129.90	00.21	45.01	2.55	02.50	139.19

# CHARACTERISTICS OF A GOOD ROLL PASS DESIGN

- To ensure a profile with a smooth surface and correct dimensions within the stipulated limits of standards.
- To ensure the minimum expense in terms of energy, power and roll consumption,
- To give deformation in such a way and at stages to have minimum internal stresses in the finished product.
- To create a simple and convenient work culture at stand, minimizing the manual operation to the minimum possible extent and to introduce the automation of technological process.
- To optimize the number of passes required for rolling to reduce the total rolling time cycle, with minimum time spent for changing and adjusting of rolls.

### **ROLL PASS DESIGN PROCESS**

- Determination of finished product dimensions.
- Calculation of steel contraction factor.
- Calculation of average elongation and number of passes required.
- Determination of appropriate pass shapes.
- Calculations of rolling power required and mechanical equipment loads.
- Determination of pass progression and family tree.
- Drawing of detailed pass shapes.

### **TYPICAL HEATING SCHEDULE**

Group	Type of steel	Temperature,OC
I	Carbon and low-alloy steels (up to 0.45% C)	1200-1220
II	Carbon, low-and medium alloy steels (up to o.65%C)	1180-1200
III	Carbon and medium alloy steel (up to 0.9%C)	1140-1160
IV	Carbon and alloy steel; tool and bearing steel (up to 1%C)	1120-1140
V	Carbon and medium alloy steel; tool and high manganese steels (up to 1.3%C)	1100-1120
VI	Nichrome and stainless steels	1200-1220
VII	High-speed steels	1180-1200



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